



Capacity II

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Evaporation

Evaporators-

Crushing rate - 100 t.c.h.

M.J.% cane - 110%

Brix of juice - 15

Brix of syrup - 60

R.J. Initial temp - 30° C.

R.J. final temp - 70° C.

S.J. initial temp- 68° C.

S.J. final temp- 100° C.

Masseccuite% Cane- $26+12+7= 46\%$



Evaporation

Evaporation rates-

V.C.- 32 kg/ m²/hr

1st - 29

2nd - 26

3rd - 24

4th - 18

Latent heats-

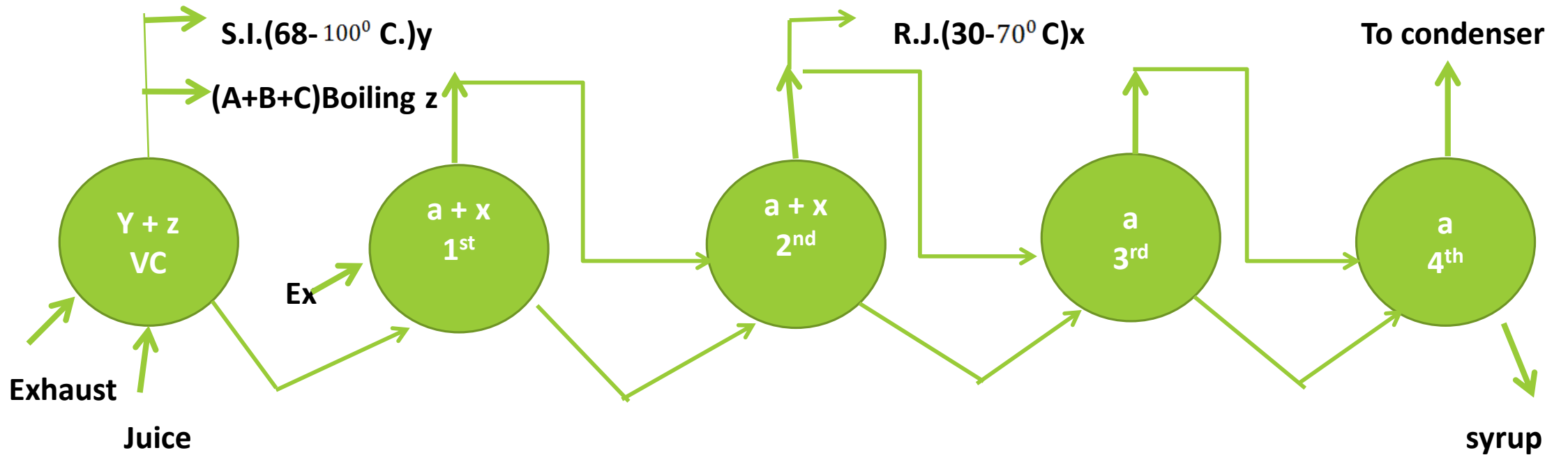
1st vapour- 532 k.cal/kg

2nd- 540

3rd -550



Evaporation





Evaporation

$$\text{Total Evaporation} = 4a + 2x + y + z = 100 \times 1.1 \left(1 - \frac{15}{60}\right)$$

$$= 83 \text{ T/hr} = 83000 \text{ kg/h}$$

$$\text{vapours for S.J.} = \frac{MS\Delta t}{532 \times 0.95} = \frac{100 \times 1.1 \times 1000 \times 0.9 (32^\circ \text{C})}{532 \times 0.95} = 6268 \text{ kg/h}$$

$$\text{Vapours for (A+B+C) boiling} = 45 \times 0.6 = 27 \text{ T/hr} = 27000 \text{ kg/h}$$

$$\text{Evaporation in V.C.} = 6268 + 27000 = 33268 \text{ kg/hr}$$

$$\text{H.S. of V.C.} = \frac{33268}{32} = 1040 \text{ s.q.m.}$$

$$\text{Evaporation in quad} = 83000 - 33268 = 49732 \text{ kg/h}$$

$$4a + 2x = 49732 \text{ Kg/h}$$



Evaporation

Value of X

$$\text{vapours for R.J.} = \frac{100 \times 1.1 \times 1000 \times 0.9(40^\circ\text{C})}{540 \times 0.95} = 7719 \text{ kg/h}$$

Now

$$4a + 2 \times 7719 = 49732$$

$$a = 8574 \text{ kg/hr}$$

H.S.-

$$4^{\text{th}} = \frac{8574}{18} = 476 \text{ sq.m.}$$

$$3^{\text{rd}} = \frac{8574}{24} = 357 \text{ sq.m.}$$



Evaporation

$$2^{\text{nd}} = \frac{8574 + 7719}{26} = 627 \text{ sq.m.}$$

$$1^{\text{st}} = \frac{8574 + 7719}{29} = 562 \text{ sq.m.}$$



Pan Capacity

Crushing rate – 3500 TCD(150 TCH)

	<u>m/c % cane</u>	<u>m/c per day</u>	<u>Boiling time</u>	<u>No. of strikes/day</u>	<u>Pan Cap.</u>
A	25	875 T	4Hrs.	6	146 T
B	11	385 T	6Hrs	4	196 T
C	8	280 T	8 Hrs.	3	93 T

For Continuous Pans for B &C massecuite

B-massecuite per/hr – 16.5 T/hr.

C-massecuite per/hr- 12 T/hr.



Crystallizer

	<u>m/c % cane</u>	<u>m/c per day</u>	<u>cooling time</u>	<u>cycles/day</u>	<u>Cryst. Cap.</u>
A	25	875 T	4Hrs	6	146 T
B	11	385 T	12Hrs	2	193 T
C	8	280 T	24Hrs	1	280 T

For Continuous Crystallisers

Holding Cap. of B - Crystalliser – 200 T

Holding Cap. of C - Crystalliser – 300 T



Crystallizer

Capacity Factor for Crystallizer = 222 ft³ / tch

Water requirement for crystallizer = 0.8 kg/kg of massecuite

$$W = \alpha v d c (T_0 - T) / (t - t_0)$$

Where,

α - Coefficient of cooling (1.20)

V – volume of massecuite m³ /hr

d- Density of massecuite

T₀ & T – initial and final temp. of massecuite

t₀ & t initial and final temp. of water



Centrifugal

	<u>m/c % cane</u>	<u>m/c per Hrs</u>	<u>curing time</u>	<u>cycles/hr</u>	<u>m/c per cycle</u>
A	25	38T	6 min	10	3.8 T
B	11	17T	15 min	4	4.25 T
C	08	12T	30 min	2	6 T

Continuous machines for B&C

O.D.(mm)

Capacity T/hr

1100

7 for B & C after curing, 4 for C fore curing

1300

10 for B & C after curing, 6 for C fore curing

1500

12 for B & C after curing, 8 for C fore curing



Centrifugal

Gravity Factor – It is ratio of centrifugal force exerted on material to that of gravity.

$$G = m \omega^2 R_m / m g$$

Where,

m - mass of the material in kg

ω - angular velocity

R_m – mean equivalent radius

g – gravitational force



Centrifugal

Screen area of batch centrifugal machine

= 0.12 m² /tch for A & B massecuite

= 0.13 m² /tch for C massecuite

- Power Consumption = 3 – 4 kw / ton of massecuite
- Water qty. required in centrifugal machine = 10 % on weight of sugar
- Steam required in centrifugal machine = 20 % on weight of sugar



Drying & Conveying

$$\text{Gross Hopper } Q = S A n k d$$

Where,

Q – out put of sugar in kg/ min.

S – cross section of hopper in m^2

A – movement of sugar / stroke in m (3 in.)

n – rotational speed in rpm (300)

K – coefficient of slip (0.5)

d – density of sugar (kg/ m^3)

Power (kw) = 2.25 + S (length * width)



Drying & Conveying

Sugar Elevator $Q = G V N$

Where,

Q – output of sugar in kg/ min.

G – weight of sugar / bucket in kg

V – speed of belt (m/ min.)

N – no. of bucket / m of belt

Distance between buckets 30 - 40 cm

Speed of belt 18 - 30 m/min.



Cooling & Condensing

Condenser water requirement,

$$W = 607 + 0.3 t_v - t_2 / (t_2 - t_1)$$

Where,

W – weight of cooling water necessary / unit weight of vapour to be condensed

t_1 , t_2 & t_v – temp. of cooling water, warm water & vapour.

Area of spray pond = 750 kg / m² /hr (of water to be treated)

Distance between pipes = 2.5 – 4 m

Distance between nozzles = 2 – 2.5 m



Cooling & Condensing

Qty. of water delivered by a nozzle $q = 0.36 c s \sqrt{2 g H}$

Where,

q – capacity of nozzle m^3 /hr

c – contraction coefficient (0.5)

S – cross section of nozzle orifice cm^2

g – gravitational force

H – pressure at nozzle in m



Cooling & Condensing

No. of nozzles $N = Q / q$

Where,

Q – total water to be cooled (m^3/hr)

q – qty of water delivered by one nozzle



THANK YOU